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SOLAR/1024-78/12

## Monthly Performance Report

LIVING SYSTEMS
DECEMBER 1978





U.S. Department of Energy

National Solar Heating and Cooling Demonstration Program

**National Solar Data Program** 

NOTICE \_

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## MONTHLY PERFORMANCE REPORT

## LIVING SYSTEMS

## DECEMBER 1978

## I. SYSTEM DESCRIPTION

The Living Systems site is a single-family residence in Davis, California. The home has approximately 1700 square feet of conditioned space. The solar energy system consists of two independently controlled systems: An active system for preheating domestic-hot-water (DHW) and a passive system for space heating the home.

The active solar DHW system has an array of flat-plate collectors with a gross area of 46 square feet. The array faces south at an angle of 45 degrees to the horizontal. Potable city water is the transfer medium used throughout the system. When water in the collector is sufficiently warmer than that in the preheat tank, the controller starts the circulation between the preheat storage tank and the collector. The preheat tank holds 82-gallons and water is supplied, on demand, to a conventional 20-gallon DHW tank. When the water preheated by solar energy is not hot enough to satisfy the hot water load, a natural gas burner in the 20-gallon DHW tank provides auxiliary energy for water heating. The system is shown schematically in Figure 1.

The passive solar space heating system is of the direct-gain type illustrated schematically in Figure 2. Incident solar energy is admitted to the building through both the large south-facing vertical windows (approximately 200 square feet) and the overhead skylight (approximately 80 square feet at 60 degrees from the horizontal). Manually operated insulating curtains provide insulation during the night and sunless days for the south-facing collector windows; manually operated insulating shutters provide night insulation for the skylight glazing and are aluminum coated to provide reflection to the space below when open. Solar energy storage is provided by bluepainted steel water-filled tubes containing approximately 3600 gallons of water placed near the south window wall and under the skylight. Additional storage is provided by the 6-inch-thick concrete slab floor of the building which is covered by brown tiles. Collected solar energy is distributed by natural convection, by conduction through the slab, and by radiation. Floor covering is minimal: linoleum in the kitchen and eating area and white shag rugs in two bedrooms. The building envelope is well insulated in order to ensure energy conservation, with R-19 insulation in the walls and R-30 insulation in the roof. The effective R-value of the window areas with curtains and shutters in place is in the range of R-2 to R-10. All glass surfaces are double-glazed with minimum window area in nonsouth-facing walls. Auxiliary space heating is provided by a gas-fired wall furnace; as with the solar heating, natural convection distributes the heat. Additional auxiliary energy can be supplied from a wood-burning stove.

Building summer overheat protection is provided by several means: First, roof overhangs over the south-facing glazed areas provide shading; second,

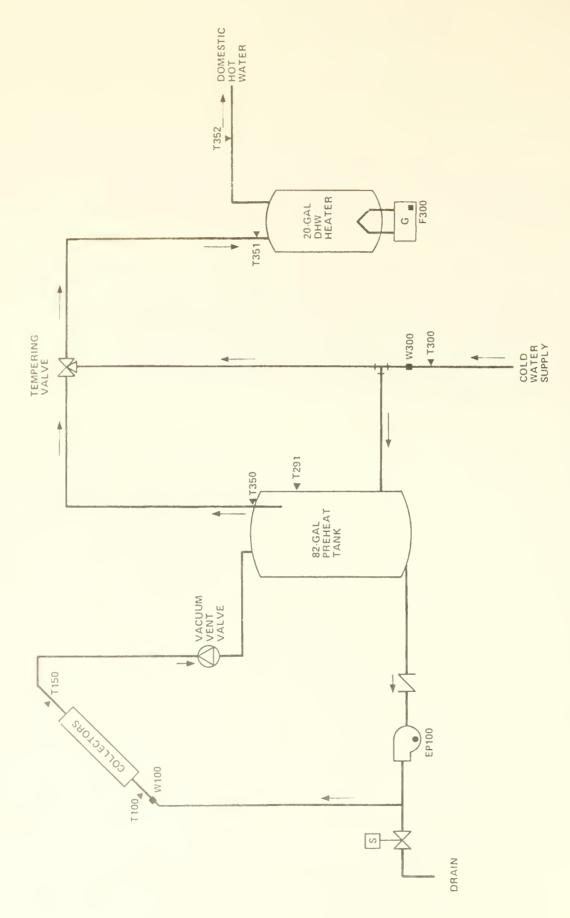
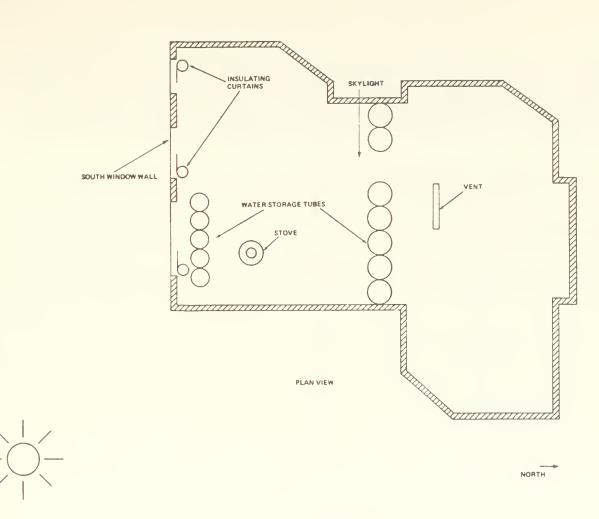


Figure 1. LIVING SYSTEMS ACTIVE SOLAR DOMESTIC HOT WATER SYSTEM SCHEMATIC



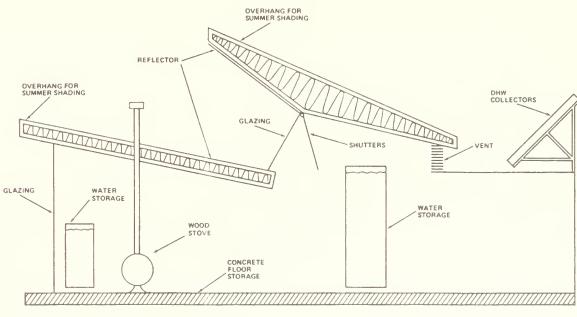


Figure 2. LIVING SYSTEMS PASSIVE SPACE HEATING SYSTEM

EAST SIDE VIEW

operable windows in the south wall along with a vent in the north wall are used for cross-ventilation of the house at night, cooling the solar storage mass and providing moderation of daytime building temperatures; third, the curtains and shutters over the windows can be closed during the day to prevent collection of incident solar energy. When necessary, a ceiling fan is available to assist distribution of heating and venting.

## II. PERFORMANCE EVALUATION

## INTRODUCTION

Performance evaluation is presented in two parts for this solar energy site: The first part covers the active solar DHW system; the second covers the passive solar space heating system.

The communications system was operable only during the last 16 days of the month and the active solar DHW system was extensively damaged by freezing on December 8. Only limited information is available on the active DHW system. The passive solar space heating system provided over 50 percent of the space heating demand during the month. Operation of the wood-burning stove during periods of low incident solar energy provided backup energy while reducing the space heating demand. Daily variations in building temperature were minimal, indicating the presence of substantial amounts of energy storage capacity. Comfort levels remained reasonable throughout the month.

## WEATHER CONDITIONS, ACTIVE SOLAR DHW SYSTEM

During the month total incident solar energy on the DHW collector array was 0.86 million Btu for a daily average of 606 Btu per square foot. This was below the estimated average daily solar radiation for this geographical area during December of 943 Btu per square foot for a south-facing plane with a tilt of 45 degrees to the horizontal. The average ambient temperature during December was 38°F as compared with the long-term average for December of 46°F.

## THERMAL PERFORMANCE, ACTIVE SOLAR DHW SYSTEM

Collector - The total incident solar radiation on the DHW collector array for the month of December was 0.86 million Btu. During the brief period of the month when the collector was operative, no information was available. During the portion of the month when the data was collected and the DHW collector was inoperative, the storage, pipes, sensors, etc. were still working. There was leakage of 0.061 million Btu from the passive heating system into the DHW preheat system, resulting in an effective collector array efficiency of 7 percent, based on total incident insolation. There was no operating energy required by the inoperative collector loop.

<u>DHW Load</u> - The DHW system consumed 0.061 million Btu of solar energy and 1.8 million Btu of auxiliary thermal energy (equivalent to 3.0 million Btu of

auxiliary fossil fuel energy) to satisfy a hot water load of 1.9 million Btu. The solar fraction of this load was 11 percent. The passive system spill-over resulted in fossil fuel energy savings of 0.10 million Btu. A daily average of 122 gallons of DHW was consumed at an estimated average temperature of 122°F delivered from the tank.

## WEATHER CONDITIONS, PASSIVE SOLAR SPACE HEATING SYSTEM

During the month, total incident solar energy on the passive collector south windows and skylight was 5.4 million Btu for a daily average of 633 Btu per square foot. This was below the estimated average daily solar radiation for this geographical area during December of 982 Btu per square foot for a south-facing plane with a tilt of 60 degrees to the horizontal. The average ambient temperature during December was 38°F as compared with the long-term average for December of 46°F.

## THERMAL PERFORMANCE, PASSIVE SOLAR SPACE HEATING SYSTEM

The total incident solar radiation on the collector windows for the month of December was 5.4 million Btu. The total solar energy for the month of December delivered to the space heating load was 4.4 million Btu, resulting in a collector array efficiency of 82 percent, based on total incident insolation. Auxiliary thermal energy of 3.7 million Btu (equivalent to 7.3 million Btu auxiliary fossil fuel energy) was added to satisfy a space heating load of 8.0 million Btu. This resulted in a fossil fuel energy savings of 7.3 million Btu. The solar fraction of this load was 55 percent. The average storage temperature for the month was  $69^{\circ}F$ .

On many days during December, the wood-burning stove was used to satisfy a measurable amount of the building load. The thermal energy derived from operation of the wood-burning stove is applied as a reduction to the building load; that is, the major difference between the building load and the space heating demand is the energy derived from operating the wood stove. During December, this renewable energy was approximately 1.9 million Btu. Assuming a wood stove energy conversion efficiency of 30 percent, this 1.9 million Btu is approximately equivalent to 21 percent of a cord of dry hardwood (such as oak). In terms of the savings of nonrenewable energy, this renewable thermal energy derived from the wood is equivalent to over 3.2 million Btu of fossil fuel energy.

The interior comfort level was given as 68°F in zone 1, the south end of the building, and 66°F in zone 2, the north end. The temperature difference occurs because comfort zone 2 is heated by conduction through the slab and walls, and by convection and infiltration associated with the doors. The cooler temperatures in the bedrooms do not seem objectionable.

### OBSERVATIONS

During the month of December, the new owner was still moving in and not fully advised of the normal usage of a passive solar home. The insulative shutters, one of the back doors, and the insulative curtains were not fully operational.

During the December 23 to December 26 holiday season, measurement values were abnormal because the wood stove overheated; the windows and vent were opened and the fan was turned on, sometimes for an extended period on cloudy days. On December 27 the thermostat was raised and fossil fuel was used to heat passive storage.

Computed comfort levels inside the building were reasonable during the entire month in both zones of the building. Zone I was the primary collection and storage area of the house. The comfort level in zone 2 was slightly lower than that of zone I due to the method of transferring heat to zone 2. Daily variations in building temperature averaged only 6°F for the month with a maximum variation of 10°F centered on 70.5°F occurring on both December 15 and 16.

The DHW system froze on December 8, apparently due to an installation problem. The drain-down controls operated properly, but sufficient water remained in the collectors to freeze and destroy them. With the collectors inoperative, considerable spill-over of solar energy occurred from the passive system during that portion of the month when data was being collected.

### **ENERGY SAVINGS**

The solar energy system provided a total fossil fuel energy savings of 7.4 million Btu. Although the DHW system was inoperative, it received an energy boost from the passive system for a fossil fuel savings of 0.10 million Btu. The space heating system contributed an energy savings of 7.3 million Btu.

## III. ACTION STATUS

The active DHW system was inoperative and requires major repair; insulative shutters and curtains require some work by the grantee or owner. Boeing has to repair the wind direction indicator and has to replace the DHW collector flowmeter by the time the DHW system is repaired.

## HEATING AND COCLING DEMONSTRATION PROGRAM SOLAR

## MCNTHLY REPORT SITE SUMMARY

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SOLAR HEATING AND COOLING DEMCNSTRATION PROGRAM

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WIND M.P.H. ることのころしっていることをなるますます。 4 Ī \* WIND ES S Ш GR Ī Ш RELATIVE HUMIDITY RCENT \u03a\$\u03a 9 Ш DAYTIME AMBIENT TEMP DEG F \*\*\*\*\*\*\*\*\*OOOO\*\*\*\*\*  $\alpha$ 444440WW WWW4444 ø AMBIENT EMPERATURE  $\Box$ ŧ 0.1 Z m G Ш  $\vdash$ DIFFUSE INSOLATICA Ø ⋖ U. . 0 ZUH M L B A O I L L L L L L Z 1 BTU/SQ TOTAL INSCLATION ⊢∃° m m 961 m U/80. 000 9 BT DAY OF MONTH =SUM G AVO S NB

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A. DENOTES NCT APPLICABL \* @Z

# SOLAR HEATING AND COCLING DEMCNSTRATION PROGRAM

## MONTHLY REPORT

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	OLAR/1046-	WIND PIND DIR	* ;	* *	* *	*	* #	*	*	* -	* *	+ *	*	*	*	*	*	* +	* *	F -}4	÷ **	*	*	*	*	*	*	*		*	N115	
	S	WIND WIND SPEED WPH	* *	* *	* *	*	* #	*	*	*	* *	+ *	*			0	9	0	0	9	0 (	0 (	•	•	0			2 • 1		2.8	,	
		AMB TEMP DEG	*	+ +	* *	*	* *	*	*	* -	* *	+ +	*															33		1 m		İ
DNI		BLDG TEMP DEG	* *     	++	* *	*	* *	*	*	* -	* *	+ +	*																	63	,	i
ACE HEAT		THERMAL USED MILLICN BTU	* * *         	* **	* *	*	* *	*	*	* -	* *	+ *	*	•12	• 04	• 14	• 13	• 1 1 1	9 0 0 0	100	α α • · ·		17	0 - 0	0	. 14	.13	02			0401	
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T.	AVIS, CAL	AVERAGE STCRAGE TEMP DEG F	* *	+ *	* *	*	* *	* **	*	* -	* +	+ *	*	(\)	0		ω	0	•	0 0	• α	• เ		- α	1	9	ω	6		68.8		
	59-2) D	CHANGE IN STORE ENERGY MILLICN	* *	+ *	* *	*	* *	*	*	*	* +	+ *	*	• 04	0.20	12	• 13	• 07		• LA C	•			000		0.03	.07	• 04	-0-387	-0.012	0202	į
	STEMS (1) DECEMBER	SCLAR ENERGY MICLICN BTU	* ;	+ *	* *	*	* #	*	*	*	* +	+ *	*	• 1	•21	• 14	• 18	. 20	0 1	0 <	0 0		000		000	• 12	.20	S	4 • 3 9 4	14	0400	į
	LIVING SY PERIOD:	SPACE HEATING LOAD MILLION BTU	* 3	÷ *	* *	*	* *	*	*	* -	钵 计	+ *	*	6 23	.25	• 29	.32	• 10 10	000	٠ ر ر		1 7	10	10	000	. 2	12	. 28	04	0.259	0405	
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\* DENOTES UNAVAILABLE DATA. © DENOTES NULL DATA. N.A. DENOTES NOT APPLICABLE

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AR/1046-78/1 AVG TOR DEG SH INCIDENT SOLAR ENERGY MILLION BTU 4 (7) 17 S m 000000000000000 S 0 Ш \* N 2 444460mm mmm4444 4 AMBEMP DA 10  $\infty$ W44WW4WWWWWWWWW m 000 (11) Z IOR IVE \*\*\*\*\*\*\*\*\*\*\*\*\*\*\* N NNMMMMMMMMMMNNNNNN m & HOU BIAHR ACE HOLD 92 L Ø E D H OZLU IL TE OE Ш BO ⋖ G CRNI 1 m Z Ö L I F BUIL AL Ü ე გ ლ ც ≥ 9 Ш S OZAU > A UILI TEI  $\Box$ S HH (11) -Ó ~ 00 59-2 MP BUILL TEN MIDNI DEG ER m ₹ R M E U III U 9 BLD CCM ZCN 000000000000000000 9 STE > .. BUILDING COMFORT ZONE \* ω  $\Box$ 000000000000000 Ø ING > <u>U</u>  $\vdash$   $\Box$ ┙ .. 0 DAY OF MON SUM G P O S AV Θ (n CC

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SOLAR HEATING AND COCLING DEMCNSTRATION PROGRAM

WCNTHLY REPORT NCRWALIZED PASSIVE SPACE HEATING

	HTG DEG DAYS	00000000000000000000000000000000000000		25
	NGRM FOSSIL SAVINGS MBTU/SQ FT		5160	166
	NOFM ELECTRIC SAVINGS MBTU/SO FT		*   V	V
	NCRN AUX THERMAL MBTU/SG FT		0	626
BER,1978	NCRN HEATING LCAC MBTU/SG FT	1 = 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	N	185
RIOD: DECEM	AVG NORM SPACE HEAT FACTOR 1000/SO FT	**************************************	] 	
EPORT PE	DAY OF MONTH		SUM	, , ,

\* DENOTES UNAVAILABLE DATA. ② DENOTES NULL DATA. N.A. DENOTES NOT APPLICABLE CATA.

